

## SPECIFICATION

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT WE, Keisuke Imai, a citizen of Japan residing at Kawasaki, Japan, Toru Yamazaki, a citizen of Japan residing at Kawasaki, Japan, Kakuji Inoue, a citizen of Japan residing at Sapporo, Japan, Setsuo Misaizu, a citizen of Japan residing at Sapporo, Japan and Yasunori Nagakubo, a citizen of Japan residing at Kawasaki, Japan have invented certain new and useful improvements in

OPTICAL TRANSMITTER AND ITS CONTROL METHOD

of which the following is a specification:-

TITLE OF THE INVENTION

OPTICAL TRANSMITTER AND ITS CONTROL METHOD

CROSS-REFERENCE TO RELATED APPLICATIONS

5           This application is based upon and claims the benefit of priority from the prior Japanese patent application No. 2002-221720, filed on July 30, 2002, the entire contents of which are incorporated herein by reference.

10       BACKGROUND OF THE INVENTION

1. Field of The Invention

          The present invention relates to an optical transmitter provided with an optical modulator of, for example, Mach-Zehnder type, and a control method of the optical transmitter.

15       More specifically, the present invention relates to an optical transmitter which is capable of effectively maintaining an extinction ratio of an optical modulator and improves the extinction ratio under given conditions, and a control method of the optical transmitter.

20       2. Description of the Related Art

          As for an optical transmitter used for an optical communication system, a direct modulation method that modulates a drive current to be supplied to a semiconductor laser in accordance with a data signal is known.

25       However, if the direct modulation method is used, there is the tendency that the influences of dynamic wavelength variations (chirping) in the optical output signal of the optical transmitter become increasingly large due to the influences of the wavelength dispersion in the optical fiber as the transmission rate becomes high. Apparently, the direct modulation method is not suitable for long-distance transmission.

30       To eliminate the problem, the study has been carried out on the use of an optical transmitter provided with a Mach-Zehnder optical modulator which does not easily cause the chirping theoretically.

35       Even if there is damping of the transmission signal in the long-distance transmission, the maintenance of the extinction

ratio is essential to the optical transmitter using the Mach-Zehnder optical modulator in order to attain the signal transmission with a predetermined level of precision.

5 FIG. 1 shows the composition of a conventional optical transmitter including a Mach-Zehnder optical modulator.

As shown in FIG. 1, a Mach-Zehnder optical modulator 20 receives the direct-current light from a LD (laser diode) light source 10. A driver circuit 40 drives the optical modulator 20 in response to the electric input signal which is externally supplied to the driver circuit 40, so that the optical modulator 20  
10 transmits the optical output signal according to the input signal concerned.

FIG. 2 shows the composition of the Mach-Zehnder optical modulator in FIG. 1. FIG. 3 is a diagram for explaining the input/output characteristics of a Mach-Zehnder optical  
15 modulator.

As shown in FIG. 2, the Mach-Zehnder optical modulator is configured so that the input light from the light source is split into two light beams on the two optical waveguide paths. The  
20 voltage as the input signal is applied to the electrode on one of the two optical waveguide paths, and the Mach-Zehnder optical modulator outputs the optical output signal. The optical output signal which is output by the optical modulator is in accordance with the modulation-characteristic curve as shown in FIG. 3.

25 When the high-speed input signal is supplied as the applied voltage of the optical modulator, the high-speed optical output signal is obtained at the output of the optical modulator.

Hereinafter, the difference in voltage between the top (peak) and the bottom (valley) in the waveform of the input  
30 signal to the Mach-Zehnder optical modulator which is capable of using a maximum range of the modulation characteristic curve will be referred to as  $V\pi$  (FIG. 3).

As indicated in FIG. 3, the extinction ratio EX mentioned above is represented by a value derived from the ratio of the  
35 maximum value  $V_H$  to the minimum value  $V_L$  in the waveform of the optical output signal of the optical modulator. Namely, the extinction ratio EX is represented by the following formula.

$$EX = 10 \times \log VH/VL \text{ [dB]}$$

When the value of the extinction ratio EX becomes poor (small), it indicates that the optical-transmission characteristics will deteriorate. Moreover, the extinction ratio EX tends to become poor (small) due to the inter-symbol interference when the bit rate becomes large.

### SUMMARY OF THE INVENTION

An object of the present invention is to provide an improved optical transmitter in which the above-described problems are eliminated.

Another object of the present invention is to provide an optical transmitter that is capable of stably supplying the optical output signal by maintaining the extinction ratio of the optical modulator even when the amplitude fluctuation of the incoming optical signal occurs due to operating point drifting, temperature changes or secular changes.

Another object of the present invention is to provide a control method of an optical transmitter that is capable of stably supplying the optical output signal by maintaining the extinction ratio of the optical modulator even when the amplitude fluctuation of the incoming optical signal occurs due to operating point drifting, temperature changes or secular changes.

The above-mentioned objects of the present invention are achieved by an optical transmitter comprising: an amplitude modulation unit performing amplitude modulation of only a one-side amplitude of a main signal with a low-frequency signal having a predetermined frequency; an optical modulator receiving an input signal generated after the one-side amplitude modulation, and modulating an incoming light in response to the received signal in accordance with a predetermined modulation-characteristic curve to output an optical output signal; and an operating point control unit applying a predetermined bias voltage to the optical modulator to control a level of the input signal substantially applied to the modulation-characteristic curve so that the one-side amplitude of the main signal is applied to a minimum portion of the modulation-characteristic

curve of the optical modulator.

The above-mentioned objects of the present invention are achieved by a control method of an optical transmitter provided with an optical modulator, comprising: performing amplitude  
5 modulation of only a one-side amplitude of a main signal with a low-frequency signal having a predetermined frequency; causing the optical modulator to receive an input signal generated after the one-side amplitude modulation, and modulate an incoming  
10 light in response to the received signal in accordance with a predetermined modulation-characteristic curve to output an optical output signal; and applying a predetermined bias voltage to the optical modulator to control a level of the input signal substantially applied to the modulation-characteristic curve so  
15 that the one-side amplitude of the main signal is applied to a minimum portion of the modulation-characteristic curve of the optical modulator.

In the optical transmitter of the present invention, when the amplitude of the input signal to the optical modulator is decreased by a certain factor, the level of the input signal to the  
20 optical modulator is substantially adjusted so that the predetermined one-side amplitude of the input signal may be applied to the minimum portion of the modulation-characteristic curve of the optical modulator. The optical output signal is generated at the output of the optical modulator by mainly using  
25 the lower portion of the modulation-characteristic curve concerned. Therefore, it is possible for the optical transmitter of the present invention to maximize under the given conditions the extinction ratio of the optical modulator that is represented by a value derived from the ratio of the maximum value (peak)  
30 to the minimum value (valley) in the waveform of the optical output signal of the optical modulator.

According to the optical transmitter of the present invention, only a one-side amplitude of the input signal to the optical modulator is taken as being the signal portion where the  
35 amplitude modulation is carried out, and the level of the input signal applied to the modulation-characteristic curve is controlled so that the single side of the amplitude of the input

signal concerned may be applied to the minimum portion of the modulation-characteristic curve of the optical modulator.

Consequently, even when the amplitude of the input signal to the optical modulator is decreased due to a certain factor, the optical transmitter of the present invention makes effective use of the minimum portion of the modulation-characteristic curve, and it is possible to maximize the extinction ratio under the given conditions.

## 10      BRIEF DESCRIPTION OF THE DRAWINGS

Other objects, features and advantages of the present invention will be apparent from the following detailed description when read in conjunction with the accompanying drawings.

15      FIG. 1 is a block diagram of a conventional optical transmitter.

FIG. 2 is a diagram showing the composition of a Mach-Zehnder optical modulator in FIG. 1.

20      FIG. 3 is a diagram for explaining the input/output characteristics of a Mach-Zehnder optical modulator.

FIG. 4 is a block diagram of an optical transmitter in the first preferred embodiment of the present invention.

25      FIG. 5 is a flowchart for explaining an operating point control operation of the optical transmitter of the present embodiment.

FIG. 6A and FIG. 6B are diagrams for explaining the operating point control operation of the optical transmitter of the present embodiment.

30      FIG. 7A, FIG. 7B and FIG. 7C are diagrams for explaining the operating point control operation of the optical transmitter of the present embodiment.

FIG. 8 is a diagram for explaining the operating point control operation of the optical transmitter of the present embodiment.

35      FIG. 9 is a diagram for explaining the operating point control operation of the optical transmitter of the present embodiment.

FIG. 10 is a flowchart for explaining another operating point control operation of the optical transmitter of the present embodiment.

5        FIG. 11A and FIG. 11B are diagrams for explaining the operating point control operation of the optical transmitter of the present embodiment.

FIG. 12A and FIG. 12B are diagrams for explaining the operating point control operation of the optical transmitter of the present embodiment.

10        FIG. 13 is a block diagram of an optical transmitter in the second preferred embodiment of the present invention.

FIG. 14 is a diagram for explaining a shutdown operation of the optical transmitter of the present embodiment.

15        FIG. 15 is a diagram for explaining a shutdown operation of the optical transmitter of the present invention.

#### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

20        A description will now be given of preferred embodiments of the present invention with reference to the accompanying drawings.

FIG. 4 shows the composition of an optical transmitter in the first preferred embodiment of the present invention.

25        As shown in FIG. 4, the optical transmitter of the present embodiment includes a light source 10 which emits a laser beam, a Mach-Zehnder optical modulator 20, and a driver circuit 40 which supplies a driving signal according to the input signal to one terminal 21 of the electrodes of the Mach-Zehnder optical modulator 20. The input signal is supplied to the optical modulator 20 via the driver circuit 40 from an external device (not shown).

30        The Mach-Zehnder optical modulator 20 modulates the laser beam emitted by the light source 10, in response to the input signal (the transmission signal) received via the driver circuit 40, in accordance with a predetermined modulation-characteristic curve of the optical modulator as shown in FIG. 3, and generates the corresponding optical output signal.

The optical output signal generated by the optical

modulator 20 is transmitted to a distant optical receiver (not shown) through the optical fiber.

5 The optical transmitter of FIG. 4 includes a low-frequency transmitter 60 which generates a low-frequency signal having a predetermined frequency  $f_0$ , and this low-frequency signal is supplied to the driver circuit 40 for operating point control.

10 For example, the frequency  $f_0$  of the low-frequency signal for operating point control is set to 1 kHz when the carrier frequency of the transmission signal is in a range exceeding 40 kHz. Namely, the frequency which is considerably low when compared with the carrier frequency of the transmission signal is used as the frequency  $f_0$  of the low-frequency signal for operating point control. In the driver circuit 40, the low-frequency signal for operating point control is further  
15 superimposed on the driving signal which is generated by the driver circuit 40 according to the input.

The optical transmitter of FIG. 4 further includes an optical coupler 30 and an operating point control circuit 50. The optical coupler 30 serves to split the optical output signal  
20 of the optical modulator 20 into two optical signals. One of the two optical signals is inputted to the operating point control circuit 50. The operating point control circuit 50 receives the low frequency signal for operating point control which is generated by the low frequency transmitter 60. The operating  
25 point control circuit 50 performs an operating point control which will be described later.

As a result of the operating point control, the operating point control circuit 50 applies a bias voltage for operating point control to another terminal 22 of the electrodes of the  
30 Mach-Zehnder optical modulator 20. In the optical transmitter of FIG. 4, the output signal of the operating point control circuit 50 and the output signal of a low-frequency superimposing control circuit 70 are combined together at an AND gate 80, and the resulting signal is applied to the terminal 22 of the optical  
35 modulator 20.

Furthermore, the optical transmitter of FIG. 4 includes the low-frequency superimposing control circuit 70. Operation of



the low-frequency superimposing control circuit 70 will be explained later together with a description of operation of the optical transmitter of the present embodiment which follows.

5       Next, a description will be given of the basic functions of the operating point control circuit 50 in the optical transmitter of the present embodiment with reference to FIG. 5 through FIG. 7C.

10       FIG. 5 is a flowchart for explaining the operating point control operation of the operating point control circuit 50. FIG. 6A is a diagram for explaining the operating point control operation, and FIG. 6B is a block diagram of the operating point control circuit 50 for explaining the same. FIG. 7A and FIG. 7B are diagrams for explaining the operating point control operation, and FIG. 7C is a block diagram of the operating point control circuit 50 for explaining the same.

15       In addition, the basic functions of the operating point control circuit 50 in the present embodiment are essentially the same as those in the external optical modulator control method disclosed in Japanese Laid-Open Patent Application No. 3-251815. Namely, similar to the composition as disclosed in the above document, the operating point control circuit 50 in the present embodiment serves to superimpose the waveform of a signal having a sufficiently low frequency onto the main signal in the upper and lower portions of the optical signal waveform.

20       The amplitude of the resulting signal after the superimposing is detected by a monitoring photodetector, and the operating point control circuit 50 in the present embodiment serves to maintain the bias voltage applied to the Mach-Zehnder optical modulator at the optimal level.

25       The diagrams of FIG. 6A, FIG. 7A and FIG. 7B, each of which corresponds to the diagram of FIG. 3, are provided to explain the basic functions of the operating point control circuit 50. As shown in FIG. 6B and FIG. 7C, the operating point control circuit 50 in the present embodiment includes a

30       photodetector (PD), a current-to-voltage converter (I/V) 51, a band-pass filter (BPF) 52, a phase comparator (PHS COMP) 53, a low-pass filter (LPF2) 54, an operational amplifier (OpAmp1)

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55, and an operational amplifier (OpAmp2) 56. In addition, the driver circuit 40 in the present embodiment includes a polarity comparator (POL COMP) 41.

5 In the control operation of FIG. 5, at step S1, the low frequency signal is generated by the low frequency transmitter 60. At step S2, the low frequency superimposing control circuit 70 is caused to change the phase of the low frequency signal according to the alpha value inputted by the alpha-switch signal in FIG. 4. When the alpha value is negative, the phase of the  
10 low frequency signal is reversed 180 degrees. Otherwise the phase of the low frequency signal remains unchanged.

This alpha-switch signal is a signal for applying selectively the upward or downward slope portion of the modulation-characteristic curve of the optical modulator 20 as  
15 indicated in FIG. 11A and FIG. 11B. Specifically, when the alpha value is positive, the upward slope portion of the modulation-characteristic curve of the Mach-Zehnder optical modulator 20 is selected. When the alpha value is negative, the downward slope portion of the modulation-characteristic curve  
20 of the optical modulator 20 is selected.

Although the absolute value of the alpha indicated by the alpha-switch signal is a numeric value in connection with control of the optical transmitter of the present embodiment, it is not related directly to the subject matter of the present  
25 invention, and a description thereof will be omitted.

Next, at step S3, the amplitude modulation (superimposing) of the transmission signal (the main signal) with the low frequency signal is carried out. That is, as shown in FIG. 6B, the polarity comparator 41 in the driver circuit 40  
30 detects the polarity of the waveform of the low-frequency signal of  $f_0$  generated by the low frequency transmitter 60. When the positive portion of the low-frequency signal of  $f_0$  is detected, the amplitude of the transmission signal is increased. When the negative portion of the low-frequency signal of  $f_0$  is detected,  
35 the amplitude of the transmission signal is decreased.

Furthermore, at step S4, the light from the light source 10, which is a laser diode, is modulated at the Mach-Zehnder optical

modulator 20 by receiving the input signal after the amplitude modulation (after the superimposing).

At step S5, the optical output signal of the Mach-Zehnder optical modulator 20 is split by the optical coupler 30 into two optical signals (first and second light beams), one of the two (the first light beam) is outputted as an optical output of the optical transmitter, and the other (the second light beam) is inputted to the photodetector (PD) of the operating point control circuit 50. For this reason, the optical output signal of the optical modulator 20 is equivalent to the optical input signal of the photodetector (LNPD INPUT LIGHT).

As shown in FIG. 6A, when the input signal on which the low frequency signal of  $f_0$  from the low frequency transmitter 60 through the driver circuit 40 is superimposed is located at the optimum point of  $V\pi$ , the top and bottom portions in the waveform of the input signal after the superimposing are exactly applied to the top and bottom portions of the modulation characteristic curve of the Mach-Zehnder optical modulator 20.

Therefore, the low-frequency signal component of the optical output signal becomes the waveform of half-wave rectification of the signal having the frequency  $f_0$ , and the average of the optical output signal is fixed to one half of the level of the voltage difference ( $V_H - V_L$ ).

Consequently, in the operating point control circuit 50 of FIG. 4, the detection signal of the optical signal (the second light beam) supplied from the optical coupler 30 and detected (step S6) by the photodetector (PD) is in the flat waveform as shown in FIG. 6B. This signal passes through the current-to-voltage converter 51 and the band pass filter 52, and the phase comparison is carried out by the phase comparator 53 with the output waveform of the low frequency transmitter 60 of the frequency  $f_0$  (step S7).

The output signal of the band pass filter 52 which is subjected to the comparison is in the flat waveform, and the output signal of the phase comparator 53 is in the flat waveform and set to the zero level. The output signal of the phase comparator 53 passes through the low pass filter 54, the

amplifier 55, and the amplifier 56, respectively, and it is supplied to the terminal 22 of the electrodes of the Mach-Zehnder optical modulator 20.

5 In this case, the bias voltage applied to the Mach-Zehnder optical modulator 20 does not change substantially. Therefore, the control operation following step S8 is not performed, but the control is returned to the step S6. In this case, the operating point where the input signal is applied to the modulation-characteristic curve of the modulator 20 remains unchanged.

10 In addition, the phase comparator 53 performs the processing which multiplies both the signals in consideration of the sign regardless of the DC component substantially. Consequently, regardless of the waveform of the low frequency signal of  $f_0$ , the output signal of the phase comparator 53 is in  
15 the flat waveform, and set to the zero level.

On the other hand, suppose the case in which an operating point drift occurs due to a certain factor as shown in FIG. 7A, and the operating point is moved in the plus voltage direction from the optimum point. In this case, the top and the bottom of  
20 the waveform of the input signal are respectively applied to the downward slope portion and the upward slope portion of the middle of the modulation characteristic curve.

The optical output signal waveform will be distorted and the component of the low frequency signal of  $f_0$  will be detected  
25 as an average of the optical output signal waveform in the opposite phase with the original low frequency superimposed signal (180 degrees out of phase). Namely, the comparison of step S7 is performed, and the result of the determination of step S8 is negative.

30 Consequently, as in the waveform chart in the upper portion of FIG. 7C, the operating point control circuit 50 detects the component of the low frequency signal of  $f_0$ , and the phase thereof is reversed by the band pass filter 52. The phase comparison with the phase  $f_0$  of the low frequency transmitter  
35 60 performed by the phase comparator 53 indicates that both the signals are in phase.

The output signal waveform of the phase comparator 53 is

changed to the waveform in which half wave rectification is performed in the right direction, and the signal will be equalized and reversed as a result of passing through the low pass filter 54, the amplifier 55 and the amplifier 56. Hence, the bias voltage in the minus direction is applied to the Mach-Zehnder optical modulator 20.

Consequently, as indicated by the arrow in FIG. 7A, the operating point where the input wave is applied is changed in the minus direction (step S10). The feedback control is performed so that the operating point is returned to the optimal position as shown in FIG. 6A.

In addition, both the signals are in phase by the phase comparator 53 in this case, as a result of multiplying mutually, the wave which always has the amplitude of only the right direction is outputted, and as a result of equalizing this and being reversed, it becomes the bias of the negative direction.

As shown in FIG. 7B, when the input wave shifts in the minus direction as a result of the operating point drift, the input wave and the signal in phase are detected in the optical coupler 30. The comparison of step S7 is performed, and the result of the determination of step S8 is affirmative.

Contrary to the above-mentioned case, as shown in the waveform chart of the lower part of FIG. 7C, from the phase comparator 53, the wave which carried out half wave rectification in the negative direction conversely is outputted.

Consequently, it is reversed by each of the amplifiers 54, 55, and 56, respectively, and the bias voltage of the plus direction is applied by the Mach-Zehnder optical modulator 20 from the operating point control circuit 50 (step S9), as indicated by the arrow in FIG. 7B, the operating point is changed in the plus direction. The feedback control is performed so that the operating point is returned to the optimal position as shown in FIG. 6A.

In addition, both the signals are in the opposite phase by the phase comparator 53 in this case, as a result of multiplying mutually, the wave which always has the amplitude of only the negative direction is outputted, and as a result of equalizing this

and carrying out manual reversal, it becomes the bias of the right direction.

Concerning the above-described control, when the amplitude of the input signal decreases as shown in FIG. 8 due to temperature changes, secular changes, etc., the control is performed so that the average waveform is applied as described above with FIG. 6A and FIG. 7A, and the optical output signal of the low frequency signal  $f_0$  may not be produced. As shown in FIG. 9, it is stabilized at the bias point where the upper and lower amplitudes of the optical output signal waveform derived from the upper and lower amplitudes of the input signal waveform are canceled each other. The component of the low frequency signal of  $f_0$  is lost, and the optical output signal is set in the flat waveform.

In this case, the extinction ratio in the waveform of the output optical signal deteriorates as in the following.

Namely, the extinction ratio in the state before degradation (for example, the state of FIG. 6A), or the state where the full range between the top (peak) and the bottom (valley) of the modulation-characteristic curve of the modulator can be used, is represented by the following formula.

$$EX = 10 \times \log VH/VL \text{ [dB]}$$

However, the extinction ratio in the state after degradation (for example, the state of FIG. 9) is represented by the following formula.

$$EXd = 10 \times \log (VH - \Delta V)/(VL + \Delta V) \text{ [dB]}$$

Hence, it is apparent that the condition:  $EXd < EX$  is met.

Thus, if the drive amplitude is fluctuated due to temperature changes, secular changes, etc., the extinction ratio deteriorates, which will cause undesired influences on the transmission characteristics.

Therefore, in the first preferred embodiment, the control operation is performed so that the extinction ratio is always kept at the maximum level.

A description will now be given of the control operation of the first preferred embodiment of the present invention with reference to FIG. 10 through FIG. 12B.

In FIG. 10, the steps S21, S22, S23, S26, S27, S28, S29, S30, and S31 are essentially the same as the steps S1, S2, S3, S5, S6, S7, S8, S9, and S10 in the flowchart of FIG. 5, respectively, and a description thereof will be omitted.

5           In the control operation of FIG. 10, at step S24, the low frequency superimposing control circuit 70 of FIG. 4 is caused to control the superimposing processing so that the amplitude-modulated transmission signal is combined with the phase-changed low-frequency signal. More specifically, when the  
10           alpha value is positive, the low frequency signal having the same frequency  $f_0$  and in phase with the low frequency signal generated by the low frequency transmitter 60 is superimposed on the transmission signal. On the other hand, when the alpha  
15           value is negative, the low frequency signal having the same frequency  $f_0$  and 180 degrees out of phase with the low frequency signal generated by the low frequency transmitter 60 is superimposed on the transmission signal.

          As shown in FIG 11A, when the alpha is positive, a part for the amplitude modulation of the top of the input wave is  
20           canceled, and the single-sided amplitude-modulation waveform including only a part for the amplitude modulation of the valley portion is obtained.

          Furthermore, at step S25, the input signal obtained by the superimposing processing of step S24 where the single-sided  
25           modulation is carried out is applied to the Mach-Zehnder optical modulator 20, and the incoming light is modulated according to the predetermined modulation-characteristic curve of the optical modulator 20.

          FIG. 11A and FIG. 11B show the waveform of the optical  
30           output signal before the control operation of FIG. 10 is performed when the input signal amplitude is decreased to be smaller than  $\sqrt{\pi}$  indicated in FIG. 3. FIG. 12A and FIG. 12B shows the waveform of the optical output signal after the control operation of FIG. 10 is performed in that state.

35           FIG. 11A shows the case in which the alpha indicated by the alpha-switch signal is +1 ( $\alpha = +1$ ). As shown in the lower part of FIG. 11A, the superimposing processing of step S24 is

performed, so that the signal having the frequency  $f_0$  and 180 degrees out of phase with the phase of the low frequency signal of  $f_0$  is superimposed on the transmission signal by the amplitude modulation. A part for the amplitude modulation of the upper part of the transmission signal is canceled, and the waveform in which single-sided amplitude modulation only of the lower part is carried out is obtained.

The optical output signal obtained by applying the bias voltage to the Mach-Zehnder optical modulator 20 at step S26 has the opposite phase to the phase of the low frequency signal of  $f_0$  after the amplitude modulation. Hence, the result of the determination of step S29 is negative.

Therefore, similar to the case of FIG. 7A and FIG. 7B, the control operation is performed so that the amplitude of the amplitude modulation portion of the bottom of the input signal becomes small in the optical output signal after light modulation.

The operating point where the input signal wave is applied to the modulation-characteristic curve is changed in the minus direction (step S31), and as shown in FIG. 12A, it is stabilized in the state where the amplitude modulation portion of the lower part of the input signal is applied to the valley portion of the modulation-characteristic wave.

FIG. 11B shows the case the alpha indicated by the alpha-switch signal is -1 ( $\alpha = -1$ ). As shown in the lower part of FIG. 11B, when the transmission signal in which amplitude modulation is carried out by superimposing processing of step S24, i.e., the signal having the frequency  $f_0$  and in phase with the low frequency signal is overlapped on the transmission signal, a part for the amplitude modulation of the lower part of the transmission signal after amplitude modulation is negated, and the waveform in which single-sided amplitude modulation only of the upper part is carried out is obtained.

The optical output signal obtained by applying the bias voltage to the Mach-Zehnder optical modulator 20 at step S26 has the opposite phase to the phase of the low frequency signal of  $f_0$  after the amplitude modulation.

Moreover, the phase of the low frequency signal is already



reversed at step S22 in this case, and the low frequency signal before reversal and the optical-output wave of the Mach-Zehnder optical modulator 20 are in phase. The result of the determination of step S29 is affirmative.

5           Therefore, similar to the case of FIG. 7B, the bias control is carried out so that the operating point where the input signal is applied to the modulation-characteristic curve is changed in the plus direction (step S30). Consequently, the control operation is performed so that the amplitude of the amplitude modulation portion of the top of the input signal becomes small  
10           in the optical output signal after light modulation.

          As a result, it is stabilized at the operating point where the amplitude modulation portion of the upper part of the input signal is applied to the valley portion of the modulation-  
15           characteristic curve, as shown in FIG. 12B.

          Thus, according to the operating point control of the first preferred embodiment, the bias control is carried out so that the predetermined one-side amplitude of the input signal is applied as the operating point to the valley portion of the modulation-  
20           characteristic curve of the Mach-Zehnder optical modulator 20.

          Consequently, as shown in FIG. 12A and FIG. 12B, the amplitude of the input signal is applied to the lower portion of the modulation characteristic curve of the optical modulator, and the non-used output-power portion  $\Delta V$  is left in the upper  
25           portion of the modulation characteristic curve.

          As described above, the extinction ratio is represented by a value derived from the ratio of the maximum value to the minimum value in the waveform of the optical output signal of the optical modulator, and rather than the variation of the  
30           numerator, the variation of the denominator more significantly affects the calculation results of the extinction ratio.

          Therefore, in order to improve the extinction ratio, it is effective to bring the lower side of the optical-output waveform near the lower-limit portion of  $V\pi$ , i.e., the valley portion of  
35           the modulation characteristic curve. As shown in FIG. 11A and FIG. 11B, it is attained by performing the superimposing of the low frequency signal to only the one-side amplitude of the input

signal that is supplied to the Mach-Zehnder optical modulator 20.

Next, a description will be given of the second preferred embodiment of the present invention with reference to FIG. 13, FIG. 14, and FIG. 15.

5           In the optical transmitter of the present embodiment, when the transmission signal (the main signal) externally supplied from the outside is in OFF state, the optical output of the Mach-Zehnder optical modulator 20 in operation is turned off without setting the light source 10 in OFF state. Hereinafter, this  
10           operation of the present embodiment will be called a shutdown operation.

FIG. 13 shows the composition of the optical transmitter in the second preferred embodiment of the present invention.

15           In FIG. 13, the elements that are essentially the same as corresponding elements in FIG. 4 are designated by the same reference numerals, and a description thereof will be omitted.

20           In addition, as shown in FIG 13, the second preferred embodiment has essentially the same composition as the first preferred embodiment, and the above-described operation of the present embodiment can be also realized using the composition of the first preferred embodiment. However, in the second preferred embodiment, the signal of the opposite phase of the signal of this low frequency  $f_0$  is always superimposed after amplitude modulation by the signal of low frequency  $f_0$  to the  
25           input signal to the Mach-Zehnder optical modulator 20, which will be described later. Therefore, the present embodiment corresponds to the case of FIG. 11A in which the alpha-switch signal is set to be positive.

30           FIG. 14 and FIG. 15 are diagrams for explaining a shutdown operation of the optical transmitter of the present embodiment.

35           Suppose the case in which a shutdown signal SD is inputted to the driver circuit 40 in the optical transmitter of FIG 13 so that the amplitude of the transmission signal is set to zero as shown in the lower portion of FIG. 14.

Similar to the previous embodiment, in the optical transmitter of the present embodiment, the amplitude modulation

of the transmission signal with the low frequency signal of  $f_0$  from the low-frequency transmitter 60 is performed. Control of the low-frequency superimposing control circuit 70 is performed so that a signal having the frequency  $f_0$  and 180 degrees out of phase with the low-frequency signal is superimposed on the amplitude-modulated transmission signal. The thus obtained input signal is supplied to the Mach-Zehnder optical modulator 20.

In this case, the transmission signal is in OFF state and does not contain the signal components of high frequencies above 40 kHz as in the previous embodiment. As shown in FIG. 14, the input signal supplied to the Mach-Zehnder optical modulator 20 contains only the low-frequency components of  $f_0$ .

Consequently, as shown in the upper portion of FIG. 14, the optical output signal of the opposite phase is obtained at the output of the optical modulator 20 with the low-frequency signal. Hence, the result of the determination of step S29 in FIG. 10 is negative.

Therefore, similar to the case of FIG. 11A of the first preferred embodiment, the predetermined bias voltage is applied to the optical modulator 20 by the operating point control operation, so that the operating point where the input signal waveform is applied to the light modulation characteristic curve is changed in the minus direction as shown in FIG. 15. The amplitude modulation portion (i.e., the input signal waveform itself) of the input signal is stabilized at the operating point where the input signal is applied to the valley portion of the light modulation characteristic curve.

Consequently, as shown in FIG. 15, the optical output signal is stabilized in the state near zero. The optical output signal of the Mach-Zehnder optical modulator 20 will be in OFF state substantially.

Thus, in the present embodiment, the optical transmitter has a comparatively simple composition, and when the main signal is in OFF state, it is possible to automatically set the optical output signal of the Mach-Zehnder optical modulator 20 in OFF state without setting the light source 10 in OFF state.

Accordingly, in the present invention, even when the amplitude of the transmission signal fluctuates due to temperature or power changes or secular changes, it is possible to always make the extinction ratio to the maximum, and the  
5 stabilization of optical-transmission characteristics is possible with the use of a comparatively simple composition.

Although it is in the tendency that the amplitude of the input signal to the optical modulator which is the output of the driver circuit decreases when the transmission rate becomes very  
10 high, according to the present invention, it is possible for the optical transmitter of the present invention to always keep the extinction ratio the optimal.

According to the optical transmitter of the present invention, only a one-side amplitude of the input signal to the  
15 optical modulator is taken as being the signal portion where the amplitude modulation is carried out, and the level of the input signal applied to the modulation-characteristic curve is controlled so that the single side of the amplitude of the input signal concerned may be applied to the minimum portion of the  
20 modulation-characteristic curve of the optical modulator.

Consequently, even when the amplitude of the input signal to the optical modulator is decreased due to a certain factor, the optical transmitter of the present invention makes effective use of the minimum portion of the modulation-characteristic curve,  
25 and it is possible to maximize the extinction ratio under the given conditions.

The present invention is not limited to the above-described embodiments, and variations and modifications may be made without departing from the scope of the present invention.  
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